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cont a component in said hollow interior having at least a first lead passing through
said plug to exit the pressure vessel, said plug encapsulating said component lead and
sealing said opening.

B1
cont 4. An improved pressure vessel comprising:
a tubular casing having an internal cavity with a circular cross section and an
opening in at least one end permitting access to said internal cavity;
a plug region adjacent said opening with a plug therein, the plug region being
necked down to match the internal cavity circular cross section; the internal cavity having
a hollow region adjacent the plug region and,
a component in the hollow interior having at least a first lead passing through said
plug to exit the pressure vessel, said plug encapsulating said component lead and sealing
said opening.

IN THE DRAWINGS

A Letter to Official Draftsperson is enclosed with three sheets of drawings having
changes marked in red for which permission is sought.

IN THE SPECIFICATION

Please replace the paragraph beginning on page 1, line 12, with the following
rewritten paragraph:

B2
Pressure vessels presently designed for oceanographic research under conditions
of high hydrostatic pressure typically employ O-ring seals. Such seals are conventionally
"piston" type or "compression" type seals. Such vessels have been employed to reach
ocean depths such as the Mariana's Trench which is 36,000 feet deep. At such depths
pressures of 18,000 psi must be accommodated. The design of the subject pressure vessel
required that the pressure vessel withstand pressures in an oil well drill hole of 10,000 psi
but with the added requirement of temperatures that reached 200 degrees centigrade. The
package was required to protect an optical component at these temperatures. Fiber optic
leads from the components had to be protected and permitted to extend through openings
in the package.

Please replace the paragraph beginning on page 2, line 30, with the following rewritten paragraph.

B3
Figure 1 is a schematic drawing of an interferometer 2 such as a Mach-Zhender interferometer, such as might be used in a hydrophone or sonar array for the detection of acoustical information. Such sensors are among the most sensitive known. Figure 2 shows the interferometer connected between a pair of optical couplers 4, 6 as a segment of a hydrophone array. Figure 3 shows the segment of the array positioned within a flexible tube or hose 8. The tube 8 would typically house many other segments (not shown) and might also carry a number of interconnecting optical fibers, electrical conductors, optical components such as optical amplifiers.

Please replace the paragraph beginning on page 3, line 7, with the following rewritten paragraph.

B4
The hose 8 might be deployed in a drill hole for oil that is potentially thousands of feet in length or towed behind a ship or deployed as a stationary array on the bottom of a sector of the ocean. In each such application, the optical and electronic components within the hose must be protected from extremes of hydrostatic or hydraulic pressures and in the case of down hole applications, from high temperatures approaching 200 degree centigrade.

Please replace the paragraph beginning on page 3, line 13, with the following rewritten paragraph.

B5
Figure 4 is an elevation view of the pressure vessel 10. The invention "Improved Pressure Vessel" of Figure 4 and its alternative embodiments in the figures subsequent to Figure 4 are for a pressure vessel capable of withstanding elevated hydrostatic pressures, and elevated temperature. The pressure vessel 10 provides a protected envelope for a variety of components such as fiber optic components including items such as optical couplers, wavelength dependent multiplexers, multi-function integrated optical components, interferometers such as Mach-Zhender and Michelson types, optical sources, optical amplifiers and electronic components for signal conditioning and acquisition as the application might require. In such applications, the components are kept at atmospheric pressure. The leads, electrical or optical are sealed in a plug at the

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ends of the vessel. In down-hole applications, the hose or tube 8 of Figure 3 has an inside diameter that imposes a budget on the outside diameter of any pressure vessels used for components within its interior. A typical maximum diameter for a pressure vessel might be slightly less than 0.2 inches for a down hole application.

Please replace the paragraph beginning on page 3, line 27, with the following rewritten paragraph.

B6

Fiber optic leads or pigtails 11a and 11b exit cap 12. The pressure vessel 10 has a tubular casing 14, typically fabricated from steel that is capable of withstanding extreme hydrostatic pressures.

Please replace the paragraph beginning on page 3, line 30, with the following rewritten paragraph.

B7

Figure 5 is a sectional view of a first embodiment of the pressure vessel 10 taken on section line A - A of Figure 4. Figure 5 shows that tubular casing 14 has an internal cavity 16 and with an opening 18 in at least one end. The length of the internal cavity 16 is shown by a bracket 16 below the internal cavity. In the embodiment of Figure 5, the opening 18 is at the left end of the tubular casing 14. The opening 18 permits access to said internal cavity 16. The internal cavity 16 has a hollow interior identified by bracket 20, and a plug region, having a position and length identified by bracket 22. The plug region is near the opening 18. A plug 24 is shown filling the plug region 22. Block 26 represents an electrical or optical component in the hollow interior 20. The component 20 has at least a first lead 28a, 28b passing through said plug to exit the pressure vessel as leads 11a, 11b. The plug 24 is shown encapsulating, the component leads 28a, 28b as they pass through the plug region to the opening 18 and the plug 24 seals the opening 18.

Please replace the paragraph beginning on page 4, line 11, with the following rewritten paragraph.

B8

As shown in Figures 5 - 7, the plug 24 is cast within the plug region 22 of the tubular casing 14 of a hard incompressible material such as a loaded epoxy resin or a ceramic adhesive. The plug 24 is circular in cross section because the tubular casing 14 is circular in cross section. It should be understood, that circular cross section tubing has

B8 cut
an advantage over other form factors at high pressure; however, if pressure and size permitted, alternative form factors could be used such as rectangular or triangular depending on the application and the requirements.

Please replace the paragraph beginning on page 4, line 22, with the following rewritten paragraph.

B9
Figure 7 is another alternative embodiment. A plug 24 is cast in the internal cavity 16 plug region 22 in which at least a portion of the plug region 22 has a necked down region identified by bracket 32 as having a cross section diminishing in diameter with distance from the opening 18. The internal cross section of the internal cavity 16 has a first enlarged region 33 along a first portion of the plug region 22. The plug region is then shown necked down in diameter along the necked down region 32 of the plug region 22. The necked down region 32 is followed by the hollow interior identified by bracket 20. The function of the necked down region is to drive the material of the plug into compression as the external hydrostatic pressure on the vessel increases. The diminishing portion or necked down region prevents the plug from moving into the hollow interior 20. Shoulder 34 in Figure 6 provides a similar function. In the embodiment of Figure 7, the plug region is shown to be necked down to a diameter that is a match for the diameter of the hollow interior 20 circular cross section. The irregular surface region 30 is shown positioned within the first enlarged region 33.

Please replace the paragraph beginning on page 5, line 3, with the following rewritten paragraph.

B10
In each of the embodiments, of Figures 5 - 7 and 9 - 10, the lead exiting the opening is at least a first optical fiber having an optical core covered by optical cladding. The cladding is covered by a protective plastic jacket. The jacket over the cladding is treated to remove the jacket over the desired portion using chemical or mechanical methods. The jacket is removed from a portion of the lead after the lead leaves the component. The portion of the jacket to be removed begins at phantom ellipse 36, and continues through a portion passing through the plug 24 to a point just below the outer surface of the plug identified by ellipse 38. The jacket is removed to permit the plug material to bond to the surface of the cladding which further perfects the hydraulic seal.

B11

Please replace the paragraph beginning on page 5, line 12, with the following rewritten paragraph.

The cap 12 is formed from a polymer material to cover and extend beyond the external surface of the plug 24 thereby forming a fluid barrier over the surface of the plug 24. Liquid Viton, a fluorocarbon elastomer, a rubber-like material, that holds at high temperature, is applied to the top or exposed surface of the ceramic adhesive to form cap 12.

B12

Please replace the paragraph beginning on page 5, line 17, with the following rewritten paragraph.

Figure 8 is an elevation view of the pressure vessel 10 having two openings in the tubular casing 14. The openings at the left and right ends permit access to the hollow interior 20, the extent of which is identified by bracket 20 in Figure 9, a sectional view taken on line B - B of Figure 8. The internal cavity 16 has a hollow interior identified by bracket 20.

B13

Please replace the paragraph beginning on page 5, line 22, with the following rewritten paragraph.

Figure 9 shows a first and second cylindrical plug 46, 48 more clearly identified in Figures 10a and 11a respectively. The first and second plugs are force fit via first and second plug region or internal cavity openings 18a and 18b into first and second plug regions identified in Figure 9 by brackets 40 and 42 in the tubular casing 14. A component 26 is shown in the hollow interior 20. The component has at least a first and or a second lead 28a, 28b.

B14

Please replace the paragraph beginning on page 5, line 27, with the following rewritten paragraph.

Each plug has an outer cylindrical surface 50, 52, the respective outer cylindrical surface 50, 52 of each plug is force fit via the plug region opening 18a, 18b of the cylindrical casing 14 into respective first and second plug regions 40, 42. As shown in Figures 10a and 11a, each plug 46, 48 has a through-hole 56, 58 that receives and passes at least the component first and or second lead 28a, 28b to a position outside of the

B14
cont. pressure vessel 10. Each plug also has a first O-Ring 44a, 44b to create a seal between the inner wall of the tubular casing 14 and the respective cylindrical plug outer cylindrical surface 50, 52.

Please replace the paragraph beginning on page 6, line 15, with the following rewritten paragraph.

In the embodiments of Figures 9 - 12, the through-holes 56, 58 in the first and second cylindrical plugs 46, 48 have an inner surface. A portion of each inner surface identified by dash lines in Figures 9, 10a and 11a is formed to have an irregular or roughened surface region for improved bonding with the ceramic adhesive plug. The irregular surface of the through-hole is a functional equivalent to the irregular surface region 30 in Figure 5 under bracket 30.

B15
Please replace the paragraph beginning on page 7, line 3, with the following rewritten paragraph.

A strain relief in the optical fiber is also necessary to protect the component from strain that results from the thermal expansion of the steel tubular casing 14 over a temperature rise to 200 degrees C. The length of the fiber strain relief on the right and left sides of component 26 are basically the same. It is important that the strain reliefs are sufficiently compliant, so that as the temperature changes and the steel expands or as pressure forces contraction, the fiber is not torn out of the component.

B16
Please replace the paragraph beginning on page 7, line 9, with the following rewritten paragraph.

Figure 12 shows plug 62 using a second O-ring 64. The plug 62 extends beyond the ends of the tubular casing 14 and is increased in diameter to form a cap lip that is driven against the edge of the tubular casing with increasing pressure.

B17
Please replace the paragraph beginning on page 7, line 12, with the following rewritten paragraph.

Figures 8 and 12 show the use of shrink tubing 68 over the end of the lip and the tubular casing to improve the seal of the joint formed at the interface of the lip and the end of the tubular casing, with increasing pressures.

B18

Please replace the paragraph beginning on page 7, line 29, with the following rewritten paragraph.

B19
The invention high-pressure vessel is the first to address the needs of the oil industries for a sensor that will withstand 10,000 psi and a temperature up to 200 degrees. No coupler produced before can meet the requirements imposed by the down-hole drilling application. Slight movement of the fibers does not change the performance of the coupler. Temperature change does change the performance of the coupler. The gases and chemicals in the hole can destroy the coupler. This package protects the coupler from those materials.

Please replace the paragraph beginning on page 8, line 4, with the following rewritten paragraph.

B20
The pressure vessel 10 package is typically placed in a liquid filled hose such as the hose 8 depicted in Figure 3. The hose is filled with a material similar to transformer oil. The hose is armored and sealed. The oil filling the hose prevents it from collapsing. The region in the hose in which the component is positioned has a hydrostatic pressure roughly equivalent to that of the region outside of the hose. The couplers are used with sound sensors such as Mach-Zehnder or Michelson interferometers that are outside of the package, however, if protection for these components is required in alternative application, the invention package can be adapted to accommodate the requirement of the larger component. Four couplers are typically used with each interferometer. Two are used with the sensor and two more with the telemetry. When an array of sensors are used, two couplers are used with each sensor.

Please replace the paragraph beginning on page 8, line 18, with the following rewritten paragraph.

B21
Referring again to Figure 12, if the strain relief 70 is coiled, the radius of the bend must be large enough to prevent evanescent light from escaping through the cladding. A hose used in a test of the subject pressure vessel 10 had a one-inch inside diameter. The outside diameter of the pressure vessel was limited to 3/16 inches. The vessel length was limited to 2 1/8 inches. The inside diameter of the body was 0.118 inches. The wall thickness was 0.035 inches. The steel used was 4130. It proved to have the strength